

Section 5. Fabrication and properties of ceramic breeder materials

## Fabrication development of $\text{Li}_2\text{O}$ pebbles by wet process

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### Abstract

Lithium oxide ( $\text{Li}_2\text{O}$ ) is one of the best tritium breeding materials. A small sphere of  $\text{Li}_2\text{O}$  is proposed in some designs of fusion blankets. Recently, reprocessing technology on irradiated ceramic tritium breeders was developed from the viewpoint of effective use of resources and reduction of radioactive wastes. The wet process is advantageous for fabricating small  $\text{Li}_2\text{O}$  pebbles from the reprocessed lithium-bearing solutions. Preliminary fabrication tests of  $\text{Li}_2\text{O}$  pebbles by the wet process were carried out. However, the density of the pebbles obtained was only 55%. Therefore, process improvement tests were performed in order to increase the density of  $\text{Li}_2\text{O}$  pebbles fabricated by this method. The improved process yielded  $\text{Li}_2\text{O}$  pebbles in the target range of 80–85% T.D. © 1998 Elsevier Science B.V.

### 1. Introduction

Investigations of fusion reactors have focused on the tritium breeding materials contained in the blanket because those characteristics will have a large effect on the reactor design. Ceramic tritium breeders such as  $\text{Li}_2\text{O}$ ,  $\text{LiAlO}_2$ ,  $\text{Li}_2\text{ZrO}_3$ ,  $\text{Li}_2\text{TiO}_3$  and  $\text{Li}_4\text{SiO}_4$  have been considered as candidates for tritium breeding materials for fusion reactors [1,2]. Particularly, lithium oxide ( $\text{Li}_2\text{O}$ ) is one of the best tritium breeders considering its high lithium density and high thermal conductivity [3,4]. A small pebble is the proposed form of  $\text{Li}_2\text{O}$  in the Japanese design of a fusion blanket in order to reduce thermal stress [5–8]. Recently, reprocessing technology on irradiated ceramic tritium breeders has been developed from the viewpoint of effective use of resources and the reduction of radioactive wastes [9]. A sol–gel or wet process method [10–12] is most advantageous for fabricating small  $\text{Li}_2\text{O}$  pebbles from the reprocessed lithium-bearing solution.

A preliminary fabrication test of  $\text{Li}_2\text{O}$  pebbles by a wet process was previously carried out. However, the maximum density of  $\text{Li}_2\text{O}$  pebbles was 55% T.D. in that test

[13]. Therefore, tests were conducted in this study to adjust modifications of the aging condition, calcination condition, thermal decomposition condition, etc. in order to increase  $\text{Li}_2\text{O}$  pebble density.

### 2. Experimental

#### 2.1. Materials

$\text{Li}_2\text{CO}_3$  powder feed stocks were obtained with a purity of 99.9% from Cerac. Polyvinylalcohol (PVA) was used as the binder for the  $\text{Li}_2\text{CO}_3$  powder.

#### 2.2. Fabrication process

An important feature of the wet process was the use of  $\text{Li}_2\text{CO}_3$  powder and PVA as starting materials to produce  $\text{Li}_2\text{O}$  pebbles. The process steps are shown as follows.

(1) Fabrication of gel-spheres: The liquid mixture of  $\text{Li}_2\text{CO}_3$  and PVA was dropped in cooled acetone through a nozzle in order to form spheres.

(2) Calcination of gel-spheres: PVA in the gel-spheres was removed leaving  $\text{Li}_2\text{CO}_3$  spheres.

(3) Thermal decomposition and sintering: The  $\text{Li}_2\text{CO}_3$  spheres were heated in vacuum to form  $\text{Li}_2\text{O}$  and then sintered.

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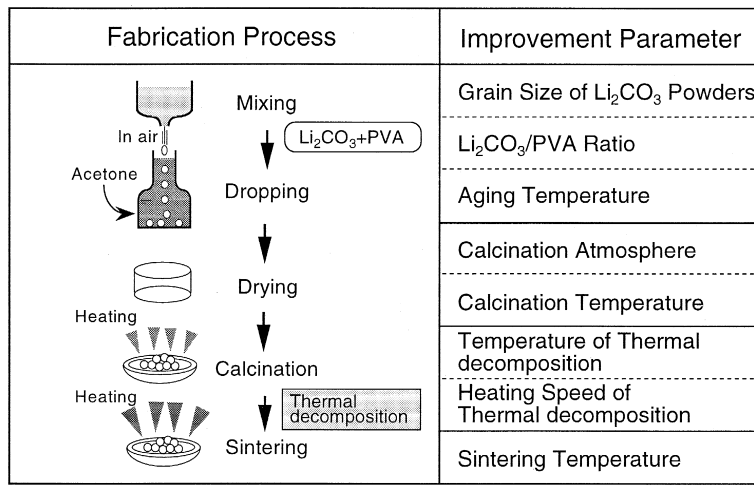


Fig. 1. A flow chart of the fabrication process of  $\text{Li}_2\text{O}$  pebbles and process improvement parameters.

A flow chart of the fabrication process of  $\text{Li}_2\text{O}$  pebbles and improvement parameters is shown in Fig. 1.

The developmental tests conducted were as follows:

In the first experiment,  $\text{Li}_2\text{CO}_3$  powder was pulverized in order to reduce the grain size from 40 to 1.0  $\mu\text{m}$ . In the process for fabrication of gel-spheres, the drop tests were carried out to decide the mixing ratio between  $\text{Li}_2\text{CO}_3$  powder and PVA. In the second experiment, the effect of aging temperature in acetone on the density of  $\text{Li}_2\text{CO}_3$  in the gel-spheres was evaluated. In the third experiment, heating tests were examined in order to remove PVA with the optimized gel-spheres and heating temperatures and atmospheres were decided. After the heating test, weight loss and growth of the grain size of the gel-spheres were measured and the crystal structure of the gel-spheres was analyzed by X-ray diffractometry (XRD). In the fourth and fifth experiments, thermal decomposition and sintering tests were carried out and the optimum condition for all

parameters (heating temperature, heating rate, pressure, etc.) was demonstrated.

### 2.3. Characterization method of $\text{Li}_2\text{O}$ pebbles

The characterization of  $\text{Li}_2\text{O}$  pebbles was performed by the methods described below. The density was measured by mercury porosimetry. The microstructure and crystalline form were determined by scanning electron microscopy (SEM) and XRD, respectively. The compressive failure load was measured using an unconfined compression tester with SiC compression indenter. The impurities in  $\text{Li}_2\text{O}$  pebbles were measured by atomic emission spectrometry with inductively coupled plasma (ICP-AES) and atomic absorption photometry and carbon content in  $\text{Li}_2\text{O}$  pebbles was measured by an infrared absorptometric method.

Table 1  
Summary of fabrication tests of  $\text{Li}_2\text{O}$  pebbles

Items	Process					
	size of $\text{Li}_2\text{CO}_3$ powders ( $\mu\text{m}$ )	aging temperature ( $^{\circ}\text{C}$ )	calcination temperature ( $^{\circ}\text{C}$ )	heating rate of thermal decomposition	sintering temperature ( $^{\circ}\text{C}$ )	density (% T.D.)
Preliminary fabrication test	<b>40</b>	20	600	R.T. $\rightarrow$ 700 $^{\circ}\text{C}$ , 1.7 $^{\circ}\text{C}/\text{min}$	1200	55
1st experiment	<b>1.0</b>	<b>20</b>	600	R.T. $\rightarrow$ 700 $^{\circ}\text{C}$ , 3.3 $^{\circ}\text{C}/\text{min}$	1100	57
2nd experiment	1.0	-20	<b>600</b>	R.T. $\rightarrow$ 700 $^{\circ}\text{C}$ , 3.3 $^{\circ}\text{C}/\text{min}$	1100	65
3rd experiment	1.0	-20	<b>400</b>	<b>R.T. <math>\rightarrow</math> 700<math>^{\circ}\text{C}</math>, 3.3<math>^{\circ}\text{C}/\text{min}</math></b>	1100	71
4th experiment	1.0	-70	400	<b>R.T. <math>\rightarrow</math> 600<math>^{\circ}\text{C}</math>, 3.3<math>^{\circ}\text{C}/\text{min}</math>, 600<math>^{\circ}\text{C}</math> <math>\rightarrow</math> 700<math>^{\circ}\text{C}</math>, 0.2<math>^{\circ}\text{C}/\text{min}</math></b>	<b>1100</b>	80
5th experiment	1.0	-70	400	R.T. $\rightarrow$ 600 $^{\circ}\text{C}$ , 3.3 $^{\circ}\text{C}/\text{min}$ , 600 $^{\circ}\text{C}$ $\rightarrow$ 700 $^{\circ}\text{C}$ , 0.2 $^{\circ}\text{C}/\text{min}$	<b>1150</b>	86

Bold type: Improvement parameters.

### 3. Results and discussions

#### 3.1. Fabrication of $\text{Li}_2\text{O}$ pebbles

A summary of fabrication tests of  $\text{Li}_2\text{O}$  pebbles is shown in Table 1. The results of each experiment in this process are described in Sections 3.1.1, 3.1.2 and 3.1.3.

##### 3.1.1. Fabrication of gel-spheres

$\text{Li}_2\text{CO}_3$  powder was pulverized and the size of the  $\text{Li}_2\text{CO}_3$  powder changed from 40 to 1.0  $\mu\text{m}$ . The fabrication tests of gel-spheres were performed under various conditions involving the mixing ratio between the  $\text{Li}_2\text{CO}_3$  powder and PVA, aging temperature and aging time in acetone. In these tests,  $\text{Li}_2\text{CO}_3$  to PVA ratios of 26 and 5 wt% were chosen as the test parameters. The sphericity of gel-spheres fabricated with the pulverized  $\text{Li}_2\text{CO}_3$  powder was better than that of gel-spheres fabricated with the  $\text{Li}_2\text{CO}_3$  powder (40  $\mu\text{m}$ ). The grain size of gel-spheres was small. In the 2nd experiment, the aging temperature was evaluated. The aging temperature dependence on the density of  $\text{Li}_2\text{CO}_3$  in gel-spheres is shown in Fig. 2. The aging time was selected as 60 min. The density of  $\text{Li}_2\text{CO}_3$  in gel-spheres increased with decreasing aging temperature between  $-20^\circ\text{C}$  and room temperature. When the aging temperature was less than  $-20^\circ\text{C}$ , the maximum density of  $\text{Li}_2\text{CO}_3$  spheres was about 55% T.D. From evaluation of aging time and temperature, an aging condition of 60 min and less than  $-20^\circ\text{C}$  was selected.

##### 3.1.2. Calcination of gel-spheres

The calcination temperature was determined for removing PVA in the gel-spheres. The gel-spheres were heated in air at each temperature (100, 200, 300, 400, 500 and  $600^\circ\text{C}$ ) for 6 h as the 3rd experiment. After heating, the gel-spheres were weighed and the grain size of the gel-spheres was observed by SEM. The relationship between calcination temperature and residual content of PVA in the gel-spheres and the relationship between calcination temperature and the grain size of  $\text{Li}_2\text{CO}_3$  particles is shown in Fig. 3. At temperatures up to  $300^\circ\text{C}$ , PVA in the gel-spheres

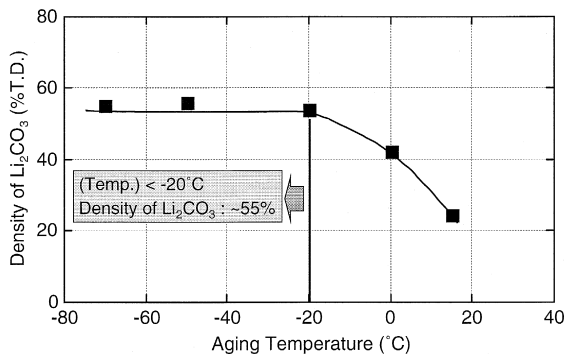


Fig. 2. Density dependence on the aging temperature of  $\text{Li}_2\text{CO}_3$  in gel-spheres.

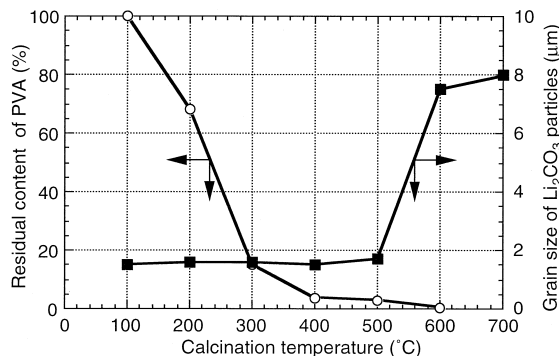
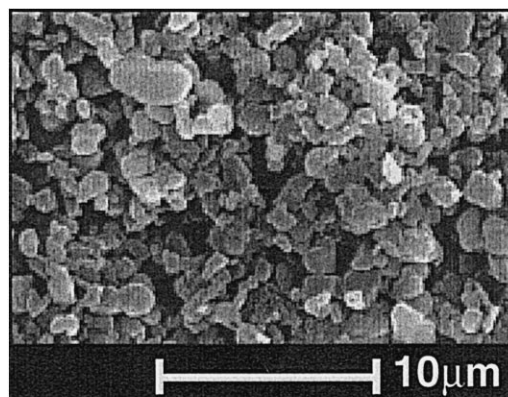
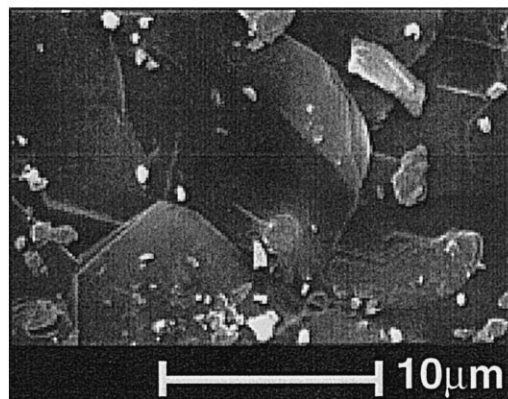


Fig. 3. Relationship between calcination temperature and residual content of PVA in gel-spheres and the relationship between calcination temperature and grain size of  $\text{Li}_2\text{CO}_3$  particles.

was not removed and the surface of the spheres was light brown. At 400, 500 and  $600^\circ\text{C}$ , greater than 95 wt% of the PVA was removed from the gel-spheres and the surface of



a)  $400^\circ\text{C}$



b)  $600^\circ\text{C}$

Fig. 4. SEM photographs of  $\text{Li}_2\text{CO}_3$  spheres after calcination showing grain growth.

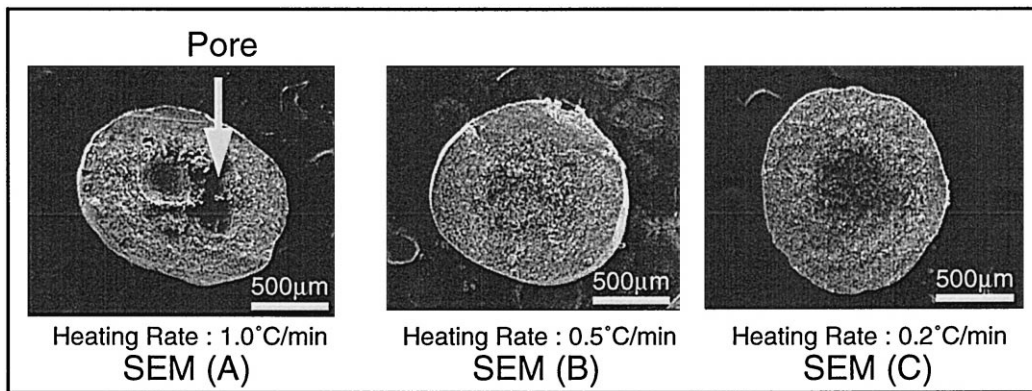
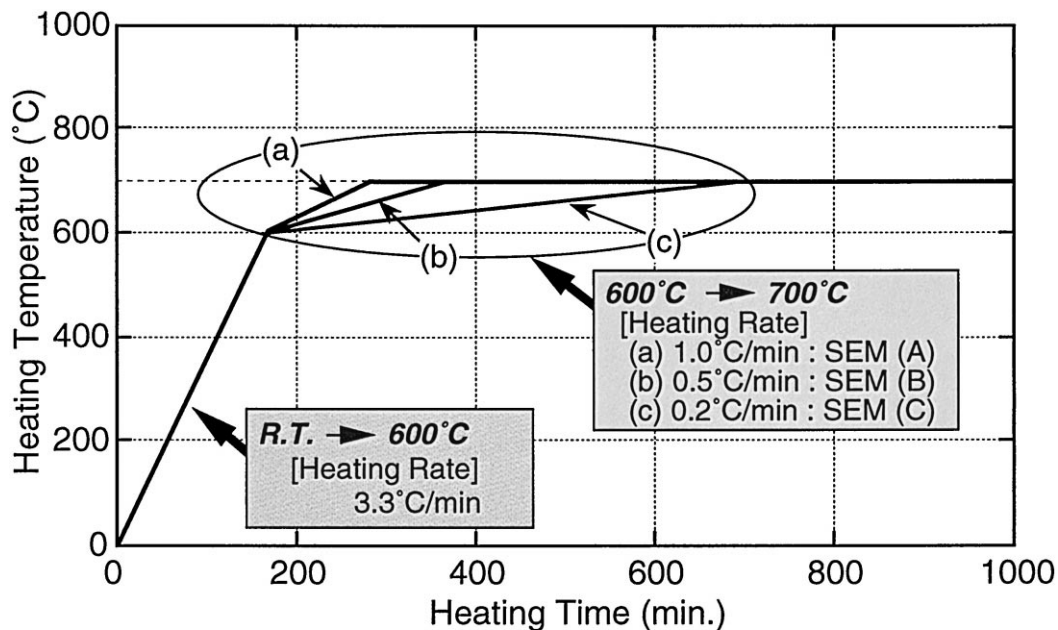


Fig. 5. Heating rate conditions during calcination and SEM photographs of Li<sub>2</sub>O pebbles after thermal decomposition.

the spheres was white. Diffraction peaks corresponding to Li<sub>2</sub>CO<sub>3</sub> were observed after heating at temperatures above 400°C. After calcination the material is referred to as ‘Li<sub>2</sub>CO<sub>3</sub> spheres’ instead of ‘gel-spheres’. SEM photographs of Li<sub>2</sub>CO<sub>3</sub> spheres after calcination are shown in Fig. 4. At 400°C in Fig. 4, the grain size of Li<sub>2</sub>CO<sub>3</sub> particles was about 1 µm. At the 600°C, the grain size of

the Li<sub>2</sub>CO<sub>3</sub> particles was about 8 µm. If grain growth affects the density of Li<sub>2</sub>O pebbles, then an optimum calcination temperature can be selected.

### 3.1.3. Thermal decomposition and sintering

The Li<sub>2</sub>CO<sub>3</sub> spheres were heated in vacuum and transformed to Li<sub>2</sub>O. The thermal decomposition of Li<sub>2</sub>CO<sub>3</sub> is

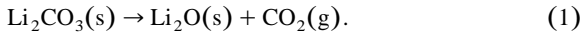
Table 2  
Relationship between sintering temperature and weight loss of Li<sub>2</sub>O pebbles

Sintering temperature (°C)	Density (% T.D.)	Weight of Li <sub>2</sub> O pebbles (g)		Weight loss of Li <sub>2</sub> O (%)
		before sintering	after sintering	
1100	80	3.6779	3.1243	15
1150	86	3.4391	2.0644	40
1200	–	5.3555	0.1383	97

Table 3  
Characterization of Li<sub>2</sub>O pebbles

Properties	Measuring methods	Measuring values
Density	liquid immersion method (Hg)	80% T.D.
Sphericity	photographic analysis	1.15 (av.) (see Fig. 6)
Crystal structure	XD analysis	XD pattern (see Fig. 8)
Pebble diameter	sieve classification	1.06 mm (av.)
Impurity content	ICP analysis	content (see Table 4)
Collapse load	autograph	1.74 kgf (av.) (see Fig. 7)

described in Ref. [14] and the transformation reaction can be written as



The Li<sub>2</sub>CO<sub>3</sub> spheres were evacuated and heated until the temperature increased to 700°C at a heating speed of 3.3°C/min. After this process, the crystal structure of the spheres was determined by XRD and Li<sub>2</sub>O was the main component detected. After thermal decomposition, weight loss of the spheres was 41.0 ± 0.4 wt%. The theoretical value obtained from Eq. (1) is 41.1 wt%.

Sintering tests were performed for 4 h at 1100°C with the Li<sub>2</sub>CO<sub>3</sub> spheres fabricated at two calcination temperatures of 400 and 600°C. When the Li<sub>2</sub>CO<sub>3</sub> spheres fabricated at 600°C were used, the size of the spheres decreased between the fabrication of the gel-spheres and calcination. From SEM photographs of Li<sub>2</sub>O pebbles, when the Li<sub>2</sub>CO<sub>3</sub> spheres were calcinated at 600°C, pores were observed in the inner part of Li<sub>2</sub>O pebbles and the density of Li<sub>2</sub>O pebbles was 65% T.D. On the other hand, the pores decreased in Li<sub>2</sub>CO<sub>3</sub> spheres calcinated at 400°C. The size of the spheres decreased after the thermal decomposition and the density of the Li<sub>2</sub>O pebbles was improved up to 71% T.D. Carbon content in the Li<sub>2</sub>O pebbles was measured by infrared absorptiometric method and was about 2 ppm. From these tests, grain growth in the Li<sub>2</sub>CO<sub>3</sub> spheres decreases the density of Li<sub>2</sub>O pebbles and, therefore, a calcination temperature of 400°C was chosen.

The calcination heating rate was evaluated in the 4th experiment. The pebble condition as a function of the

heating rate during thermal decomposition and SEM photographs of Li<sub>2</sub>O pebbles after thermal decomposition is shown in Fig. 5. Pores were observed in the inner part of Li<sub>2</sub>O pebbles when the temperature increased to 600°C at 3.3°C/min and porosity increased from 600 to 700°C at 1.0°C/min. However, pores decreased in the inner part of Li<sub>2</sub>O pebbles when the temperature increased from 600 to 700°C at a heating rate of less than 0.5°C/min. It appears that the internal homogeneous structure of Li<sub>2</sub>O pebbles can be attributed to performing the thermal decomposition reaction at the slower rate.

Sintering was conducted in vacuum at a temperature range of 1100 to 1200°C for 4 h for the 5th experiment. The relationship between the sintering temperature and weight loss of Li<sub>2</sub>O pebbles is shown in Table 2. As the sintering temperature increased, the density of Li<sub>2</sub>O pebbles also increased. At a sintering temperature of 1200°C for 4 h, Li<sub>2</sub>O was almost completely evaporated. The density and weight loss of Li<sub>2</sub>O pebbles were 80% T.D. and 15 wt% at 1100°C for 4 h, respectively. On the other hand, the density and weight loss of Li<sub>2</sub>O pebbles were 86% T.D. and 40 wt% at 1150°C for 4 h, respectively.

### 3.2. Characterization of Li<sub>2</sub>O pebbles

A characterization of Li<sub>2</sub>O pebbles fabricated in the fourth experiment was carried out. A summary on the characterization of Li<sub>2</sub>O pebbles is shown in Table 3. The main features are discussed below.

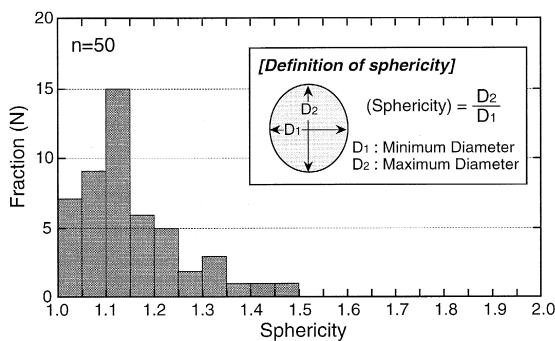


Fig. 6. Distribution of sphericity of Li<sub>2</sub>O pebbles fabricated in the 4th experiment.

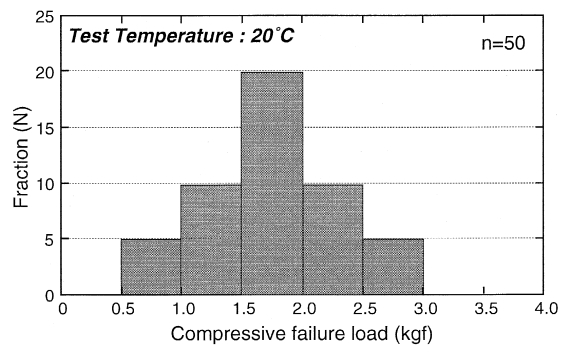


Fig. 7. Distribution of compressive failure load of Li<sub>2</sub>O pebbles fabricated in the 4th experiment.

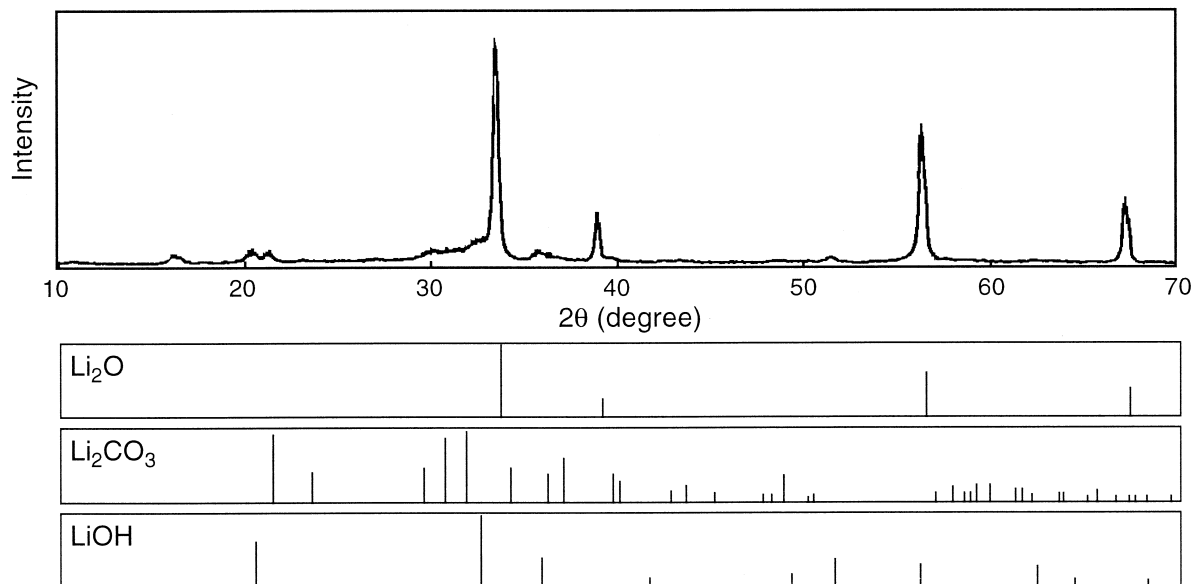


Fig. 8. X-ray diffraction pattern of Li<sub>2</sub>O pebbles.

The density of Li<sub>2</sub>O pebbles fabricated by this method was 80% T.D. The average size of Li<sub>2</sub>O pebbles was  $1.06 \pm 0.05$  mm. Sphericity of the Li<sub>2</sub>O pebbles, which is the ratio of maximum to minimum diameter, was measured using a photographic analysis method. The distribution on the sphericity of Li<sub>2</sub>O pebbles fabricated in the 4th experiment is shown in Fig. 6. The average sphericity of Li<sub>2</sub>O pebbles was  $1.15 \pm 0.10$  and the Li<sub>2</sub>O pebbles are very spherical from Fig. 6. The distribution of a compressive failure load of Li<sub>2</sub>O pebbles fabricated in the 4th experiment is shown in Fig. 7. The average compressive failure load was  $1.74 \pm 0.51$  kgf. The X-ray diffraction pattern of Li<sub>2</sub>O pebbles is shown in Fig. 8. From XRD analysis, Li<sub>2</sub>O was the main component detected. The chemical composition of Li<sub>2</sub>O pebbles is shown in Table 4 and

Table 4  
Chemical composition of Li<sub>2</sub>O pebbles

Elements	Contents (ppm)
Na	< 10
Mg	12
Ca	26
Fe	16
Cr	2
Ni	< 5
Al	60
Si	120
Pt	< 10
Cu	2
Bo	< 0.5
B	< 5
U	< 0.1

aluminium and silicon were the highest impurities detected.

From the results of these tests, potential methods for fabricating small Li<sub>2</sub>O pebbles with reasonable density were obtained.

#### 4. Conclusion

Process improvement tests for making small Li<sub>2</sub>O pebbles were carried out by a wet process in this study. The main conclusions are as follows.

(1) The density of Li<sub>2</sub>O pebbles was a function of aging temperature, calcination temperature, heating rate during thermal decomposition and sintering temperature. Careful control of aging temperature, calcination temperature, heating rate and sintering temperature were required to increase the density of Li<sub>2</sub>O pebbles.

(2) The heating rate during thermal decomposition increased the Li<sub>2</sub>O pebble density. When the temperature increased to 600°C at 3.3°C/min and increased from 600 to 700°C at less than 0.5°C/min, pores decreased in the inner part of Li<sub>2</sub>O pebbles and the Li<sub>2</sub>O pebbles had a homogeneous structure. In this test, densities of Li<sub>2</sub>O pebbles were obtained in the target range of 80 to 85% T.D.

(3) The characterization of Li<sub>2</sub>O pebbles fabricated using the optimized parameters was carried out. The average size of Li<sub>2</sub>O pebbles was 1.06 mm and the resulting sphericity was 1.15, with 1.0 being a perfect sphere.

From the results of these tests, Li<sub>2</sub>O pebbles were fabricated with a density in the target range and bright

prospects exist concerning the fabrication process of small  $\text{Li}_2\text{O}$  pebbles by this wet method. In the future, fabrication processes of other ceramic breeders such as  $\text{Li}_2\text{TiO}_3$  will be established and an automatic-control dropping system of gel-spheres will be designed and developed for a mass production process.

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